

NASA Electronic Parts and Packaging (NEPP) Program

# Lessons Learned from Screening and Qualification of COTS Capacitors

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# List of Acronyms

<b>AEC</b>	Automotive Electronics Council	<b>MSL</b>	moisture sensitivity level
<b>BI</b>	burn-in	<b>PST</b>	power surge test
<b>DCL</b>	direct current leakage	<b>PWB</b>	printed wiring board
<b>DLA</b>	Defense Logistics Agency	<b>RB</b>	reverse bias
<b>EM</b>	electrical measurements	<b>RVT</b>	random vibration test
<b>ER</b>	established reliability	<b>S&amp;Q</b>	screening and qualification
<b>ESA</b>	European Space Agency	<b>SS</b>	sample size
<b>ESR</b>	equivalent series resistance	<b>TC</b>	temperature cycling
<b>FR</b>	failure rate	<b>TS</b>	thermal shock
<b>IDC</b>	inter-digitated capacitor	<b>TTF</b>	time to failure
<b>LAT</b>	lot acceptance test	<b>VR</b>	voltage rating
<b>LT</b>	life test		

# Abstract

A traditional approach to screening and qualification of hi-rel COTS capacitors and its limitations are analyzed. Results of testing of four types of COTS capacitors for L2 projects are summarized. The types include DLA drawing tantalum MnO<sub>2</sub> capacitors, high-voltage hermetically sealed polymer tantalum capacitors, multianode COTS+ capacitors, and feedthrough BME ceramic capacitors. Lessons learned from this experience might accelerate processes and reduce risks of inclusion of COTS components in space projects.

# Outline

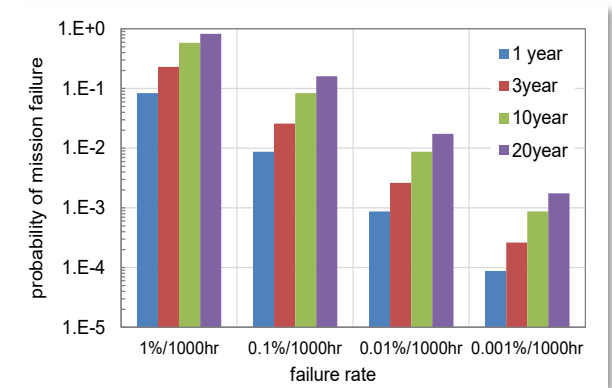
- ❑ Traditional approach to screening and qualification of hi-rel COTS capacitors and its limitations
- ❑ Case 1: DLA drawing MnO<sub>2</sub> capacitor
- ❑ Case 2: High-voltage hermetically sealed polymer tantalum capacitors
- ❑ Case 3: Multianode COTS+ tantalum capacitors
- ❑ Case 4: Feedthrough ceramic capacitors
- ❑ Lessons learned

# COTS vs. MIL-Grade Capacitors

- ❑ Capacitors for different level space projects are selected based on reliability/FR grading.
- ❑ Risk of using a COTS capacitor:  
 $P_m \times (\text{consequences of failure})$ .

$$P_m = 1 - \exp(-\lambda_m t_m), \quad \text{derating} \rightarrow \lambda_m = \lambda/AF$$

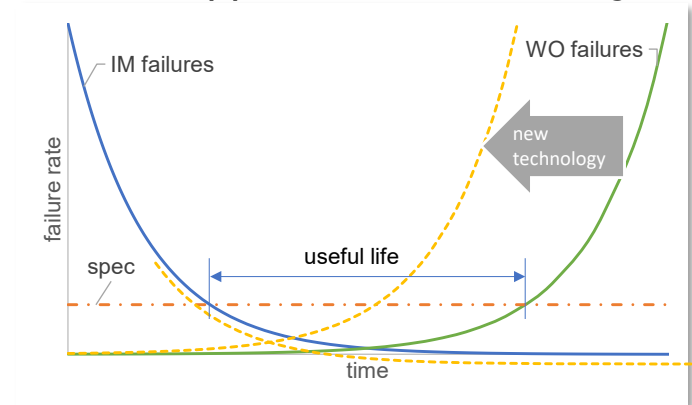
- ❑ The major benefit of using ER MIL-grade parts is that they are assumed to be acceptable for most space projects if operating conditions are within the MIL range of temperatures and voltages.
- ❑ Lack of confidence in consistency of quality in different lots of COTS capacitors → difficulties in reliability assessments for a given part type.
- ❑ Contrary to MIL applications, space projects are often interested in a single lot of capacitors that are to be used at a relatively benign conditions → the need to assess reliability of a particular batch for a specific application.
- ❑ Existing guidelines for S&Q of COTS parts typically follow MIL-spec requirements developed for relatively old technologies.



# Life Testing of COTS Capacitors

- ❑ Increasing risks of WO failures for new technology capacitors can be managed.
- ❑ If a COTS part can pass the relevant MIL spec requirements is it as good as a MIL part?
  - Due to a small SS during LT and low confidence/trust in quality consistency for COTS it is impossible to get acceptable FR without significant acceleration.
  - Test results cannot be generalized for a given part type → each lot should be tested.
  - Existing LT for COTS capacitors is a quality compliance, but not a reliability test.
  - LT conditions in the existing guidelines might be not applicable for advanced COTS.
- ❑ If COTS capacitors fail MIL requirements for life testing, can it still be used? If not, but you wish to use the part very much, then should we:
  - A. Relax the requirements in the MIL spec (IDC, hybrids)?
  - B. Assess acceleration factors and prove reliability for the mission?

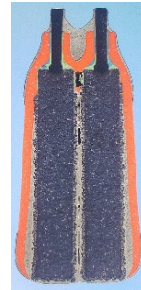
*The beauty of WO failures: PoF approach and modeling*



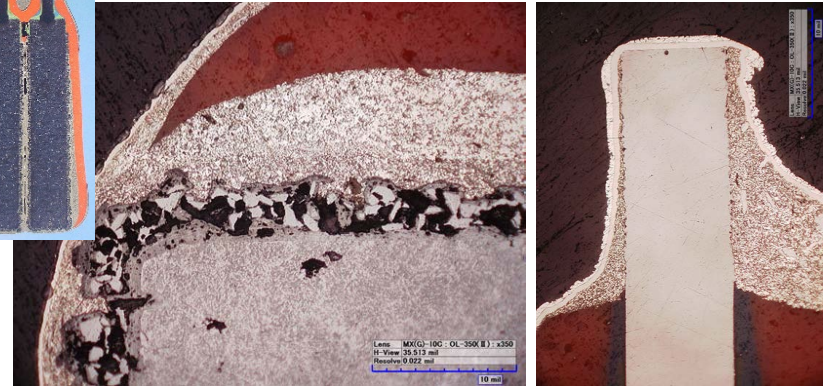
# DLA #13008

## Benefits of frameless design:

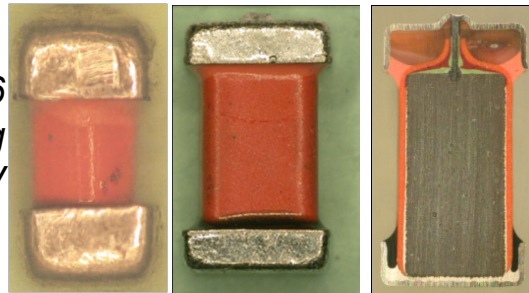
- Better polarity indication
- Elimination of wire welding
- Extended range
- The part has a good self-healing capability (10% of damage after scintillation breakdown)



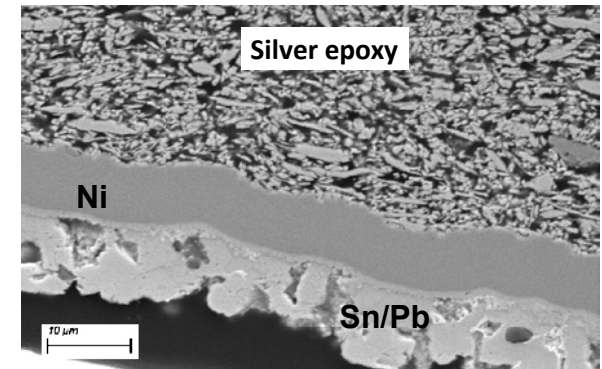
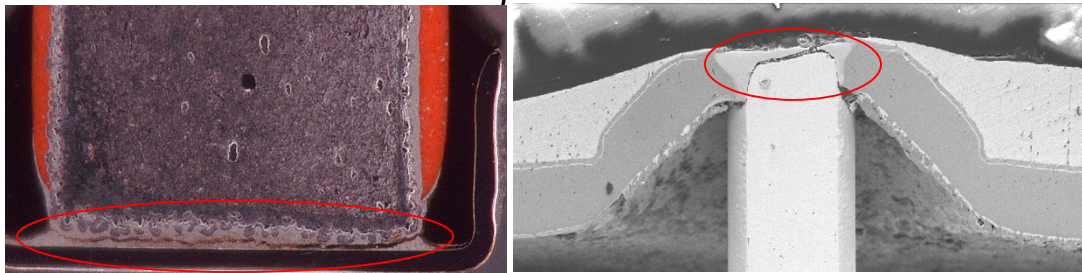
T97 max rating 22uF, 250 mΩ, 63V



CWR06  
max rating  
4.7uF, 1.5Ω, 50V



Examples of cracking at the anode and cathode in CWR06 capacitors



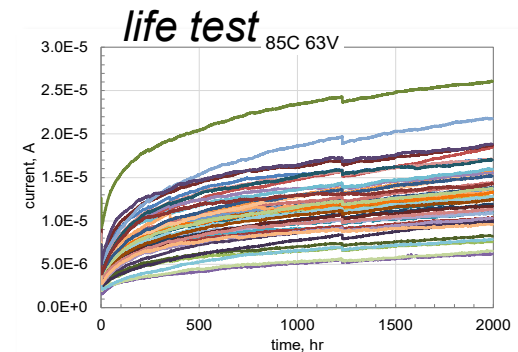
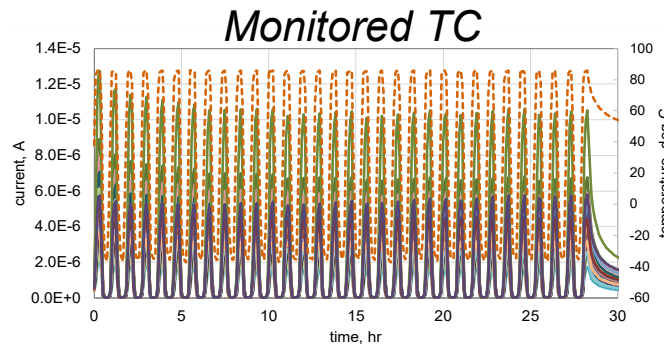
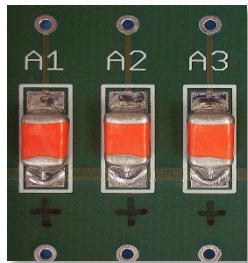
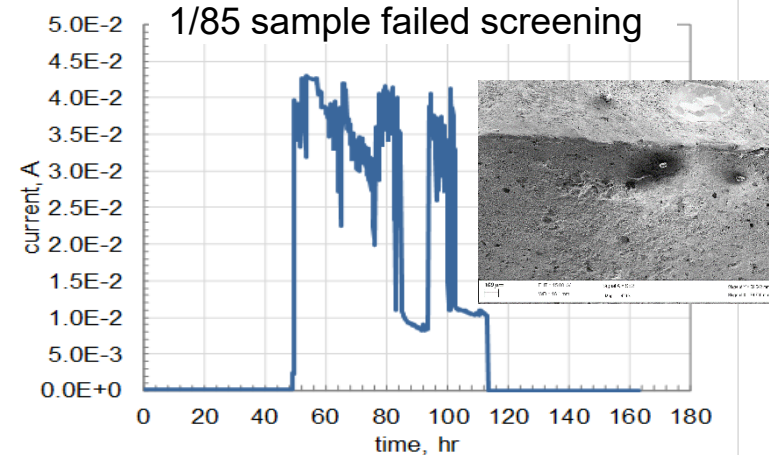
## Potential problems:

- Integrity after soldering
- Insufficient screening (85C/40hr/VR)
- Life test is optional (85C/2000hr/VR)



# DLA #13008 10uF 63V S&Q

- ❑ Application conditions for a project: 28V, survival T range from  $-25^{\circ}\text{C}$  to  $65^{\circ}\text{C}$ ; possible transients during power-up 2-5 ms.
- ❑ Screening verification included monitored BI at 85C 63V for 160hr. One out of 85 samples failed after 50 hours. The appearance of the failure site suggested scintillation breakdown.
- ❑ Qualification tests using 45 samples reflow soldered onto test PWB: monitored cycling (30 TC  $-35$  to  $+85\text{C}$ ), power surge, and life test (2000hr, 85C).

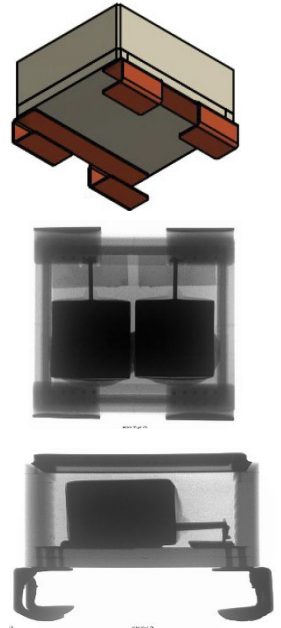


- ✓ The frameless technology improves performance and quality of the parts.
- ✓ DLA drawing parts might require BI verification.
- ✓ Life test at 85C 63V for 2khr corresponds to  $>1000\text{yr}$  during the mission.



# TCH Capacitors

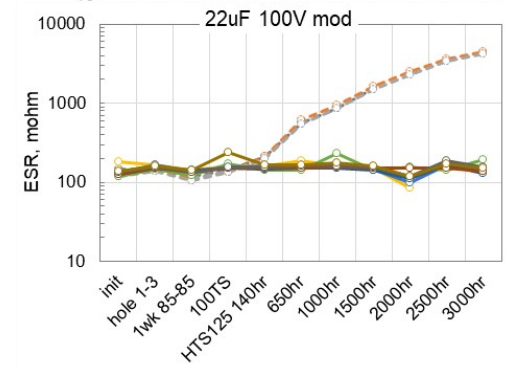
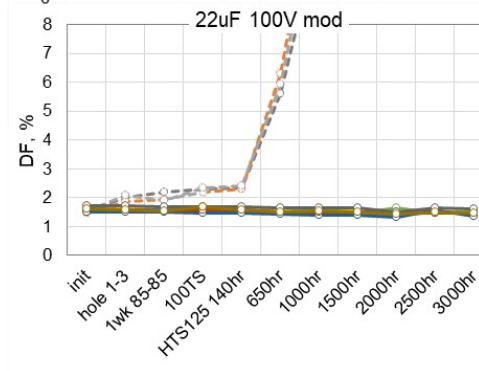
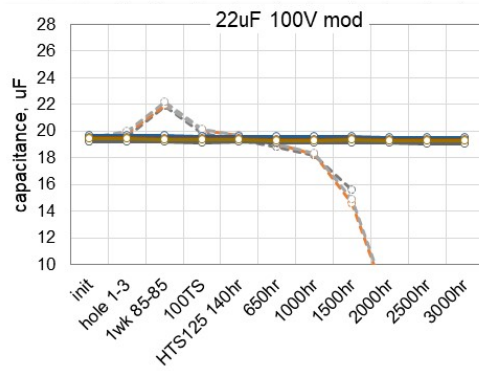
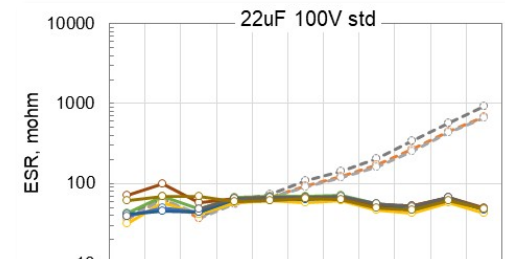
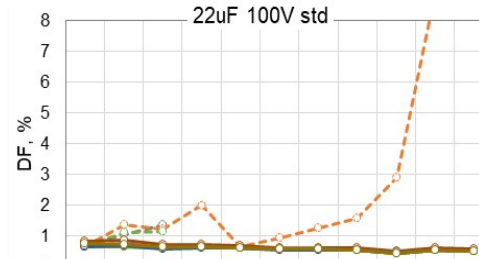
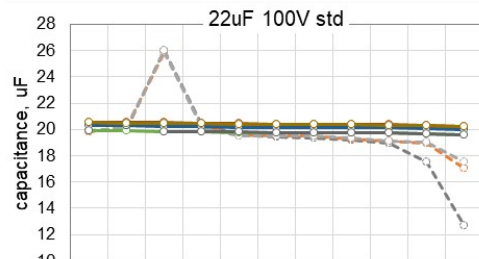
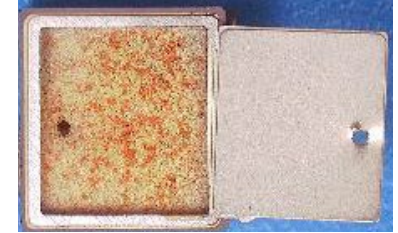
- ❑ A project selected 22 $\mu$ F 100V Ta caps to be used in 35V power lines with possible transient spikes up to 43V. Turn ON/OFF cycles are relatively slow,  $\sim$ 300  $\mu$ sec. Operational T  $\sim$  25 °C and possible variations -20 to +30 °C. Ripple currents below 20 mA, which is  $\sim$ 10 times below the specified limit.
- ❑ TCH series are hermetically sealed polymer Ta caps developed for space applications per ESA requirements.
- ❑ C-shape terminals were selected to reduce stresses from PWB.
- ❑ Screening of 420 samples included:
  - 5 TC (-55C to +125C), power surge, hermeticity, and monitored BI (85C/100V/168hr).
- ❑ LAT was carried out for 3 groups after reflow soldering onto test PWB or soldering simulation.
  - Gr.I (20pcs): 100TC -55 to +125C -> EM -> humidity (85C/85% RH/2wk) -> EM -> power surge cycling.
  - Gr.II (20pcs): reflow soldering -> EM -> stability at HT and LT -> RVT.
  - Gr.III (60pcs): reflow soldering ->EM -> monitored life test (85C/100V/2000hr)



- ✓ Potential problems:
  - Dehermetization or excessive leak
  - Reverse bias pulses
  - Reliability at operating conditions

# Effect of Dehermetization

- ❑ Small holes were drilled in several engineering samples of the part.
- ❑ AC characteristics were measured after dehermetization, exposure to moisture, 100 TS, and HTS125 up to 3000 hours.

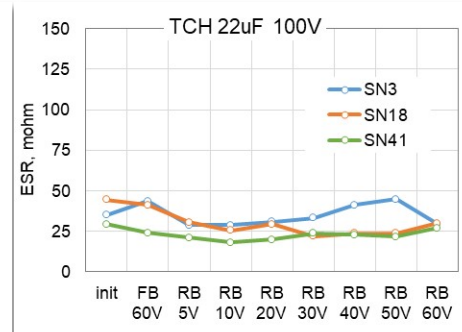
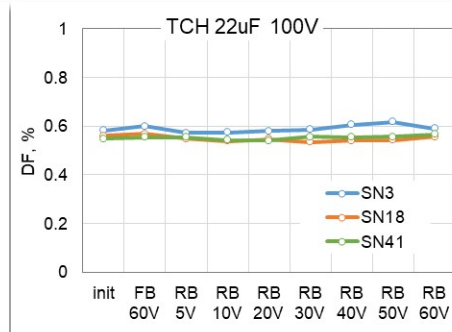
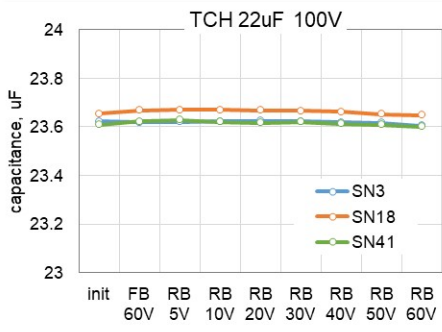
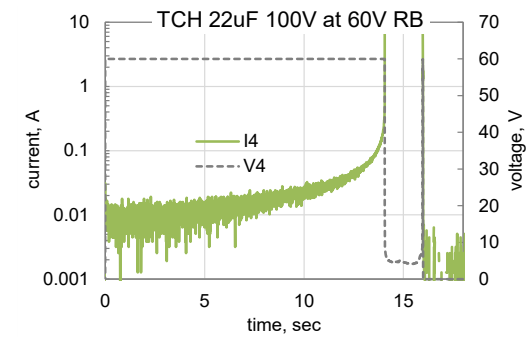
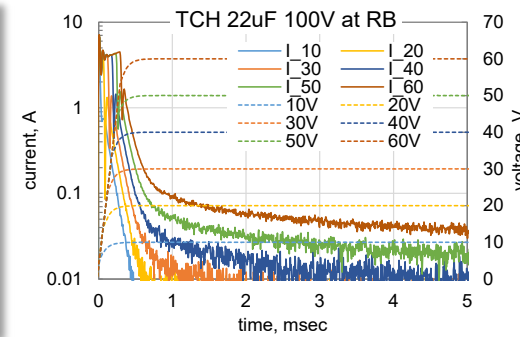
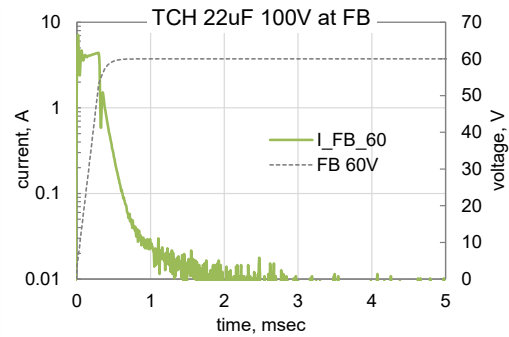


- ✓ Significant capacitance variations in non-hermetic parts indicate moisture presence.
- ✓ Epoxy foam inside the package does not substantially delay moisture penetration.
- ✓ The level of moisture corresponding to RC does not degrade the parts.
- ✓ Hermetically sealed parts can withstand > 3000hr of HTS125, whereas non-hermetic parts can fail even after 1000hr due to thermo-oxidative degradation of PEDOT/PSS.

# Effect of Reverse Bias Pulses

- During PST, the parts were stressed by 60V 0.5 sec pulses with a ramp time < 0.3msec.
- Similar pulses in reverse polarity were applied at increasing voltages.
- The currents were also monitored at 60V RB.

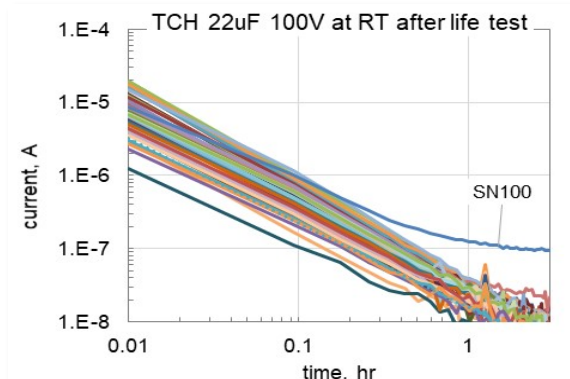
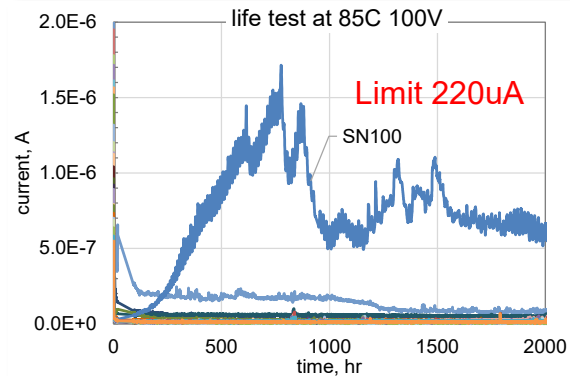
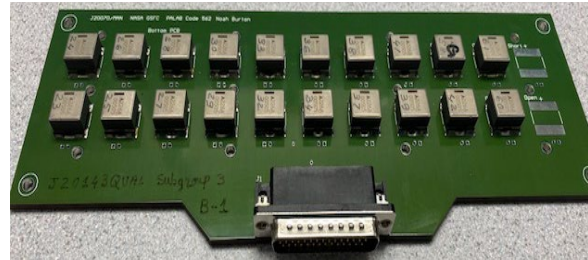
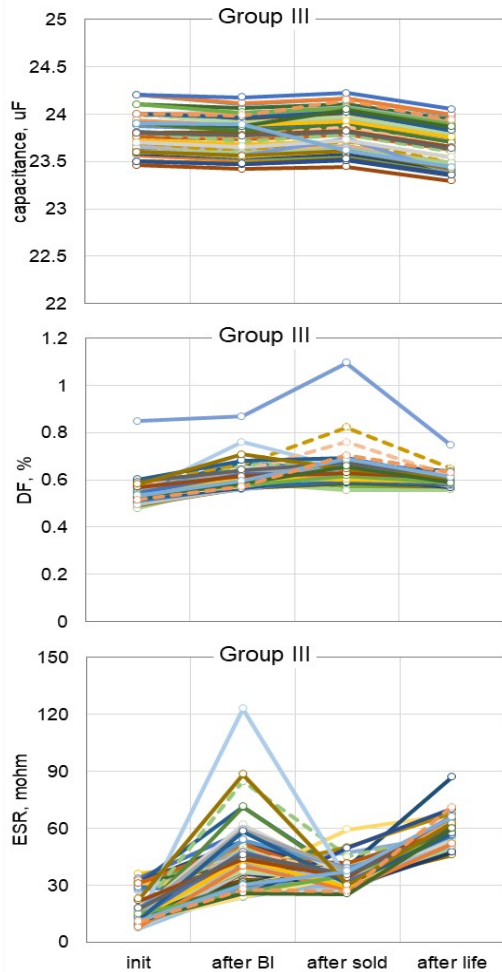
*RB failure at 60V*



- Reverse bias during PST does not damage the part.
- At 60V, failures at reverse bias can be observed after 10 sec.
- RB failures result in charring of polymer around the whole surface of the slug.

# Results of Life Testing (Gr. III, 60 pcs)

Variations of AC characteristics through the testing

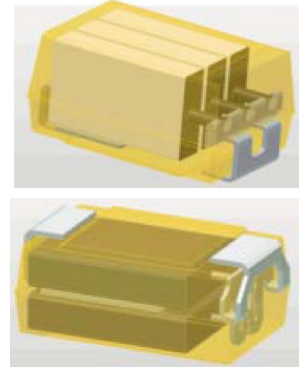


- ❑ Screening: 4.3% of 420 pcs failed DCL before BI and 0.7% failed during BI.
- ❑ Life test:
  - No failures or significant anomalies during monitored life testing.
  - No parametric degradation or failures after life testing.

✓ Conservative estimations show that 2khr life test at 85C, 100V corresponds to more than 1000 years during the mission.

# Evaluation of Multianode TBM Capacitors

- ❑ Multianode capacitors allow for a substantial reduction of ESR that can be reduced to 35-70 mohms for MnO<sub>2</sub> capacitors.
- ❑ Available with Weibull Grade “B” reliability (0.1%/1000hr).
- ❑ Potential reliability problems:
  - Greater risk of popcorning due to increased number of edges.
  - Greater risk of breakdown due to a larger surface.



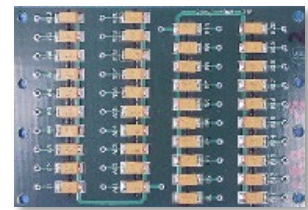
*Preliminary tests showed that multianode capacitors preconditioned per MSL1 have cracks after reflow soldering*



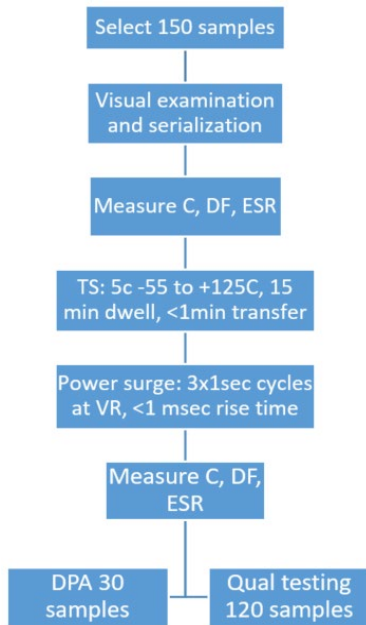
- ✓ Soldering of 6 types of TBM capacitors (720 pcs) shows that with proper baking the parts can be safely soldered onto PWBs.



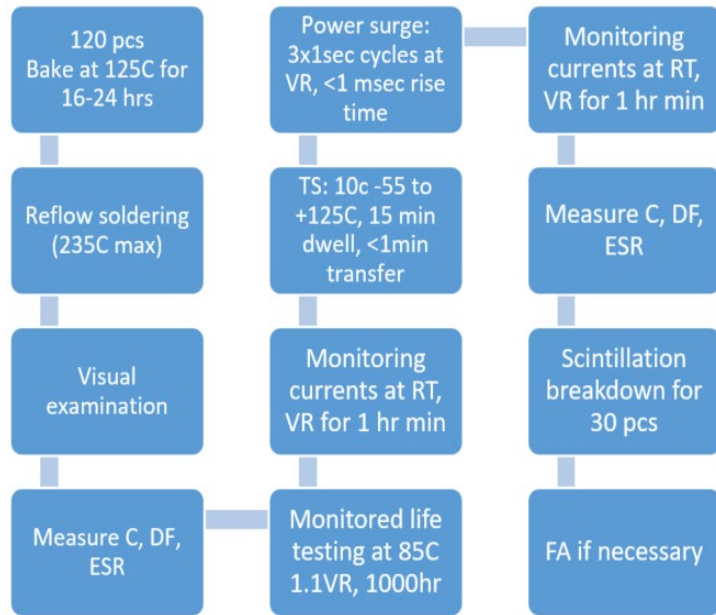
# LAT of Multianode Capacitors



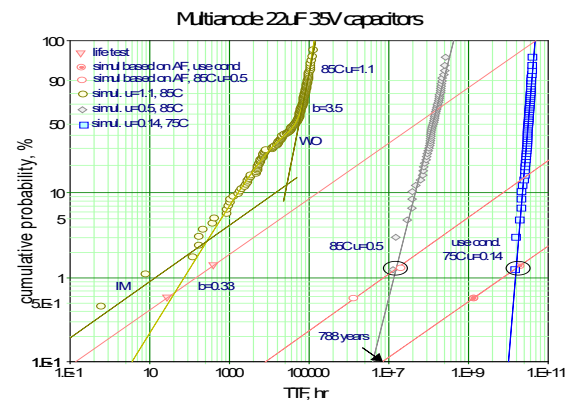
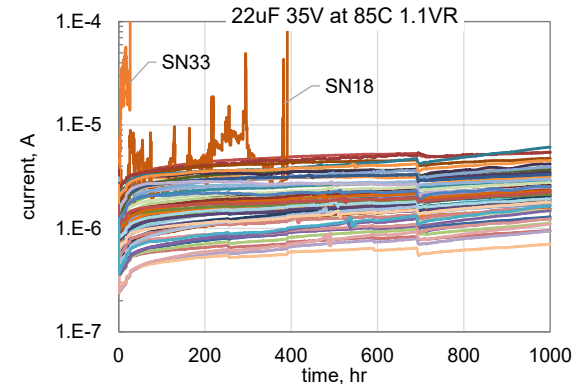
## Test flow



## Qualification tests



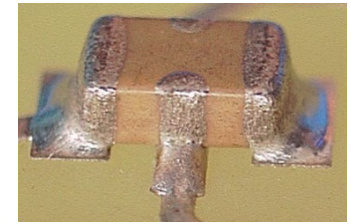
## Life Test for a Failed Lot



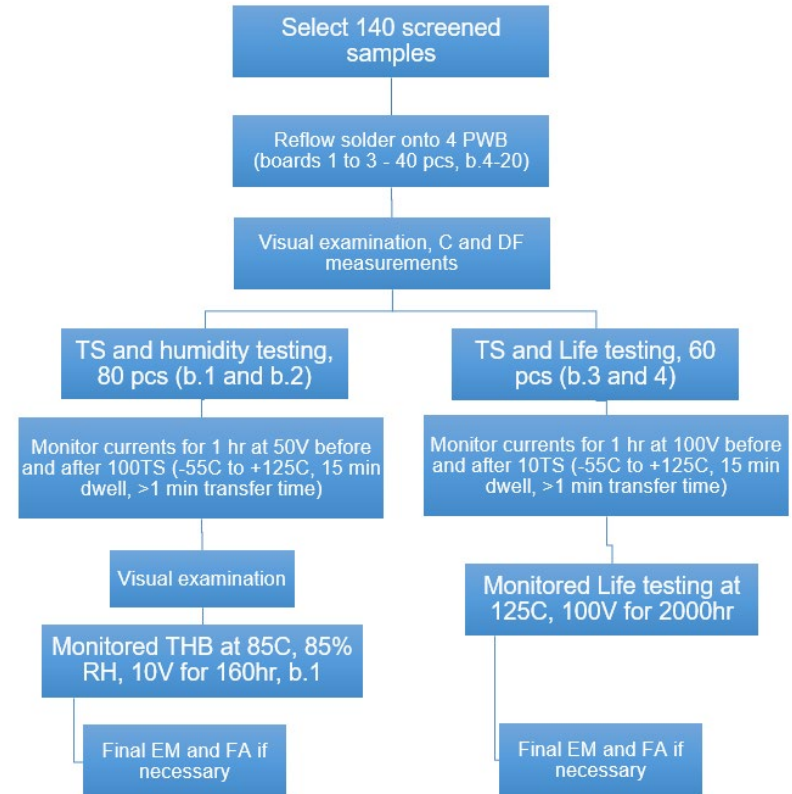
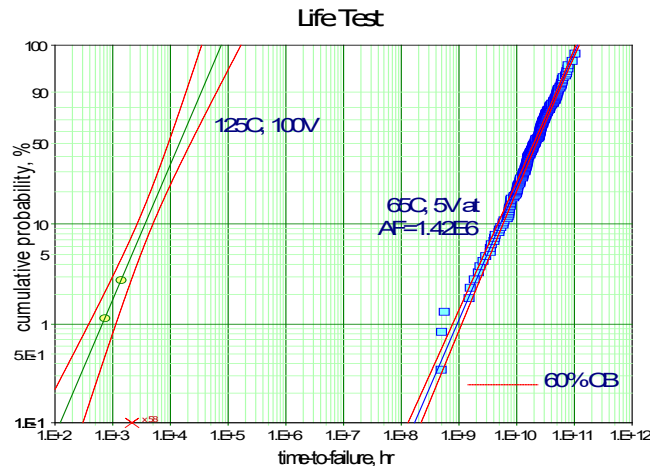
- No failures in 5 lots of capacitors.
- In one lot, 2 out of 120 samples failed life test.

- ✓ Additional screening (BI) might be necessary in one of 6 tested lots.
- ✓ Using a 45(1) criterion per the guidelines, would have 83% chance of passing life test.
- ✓ Parts that passed the life test 120(0) at 1.1VR will have the probability of failure during a 20 year mission < 0.01%.

# Feedthrough BME Capacitors



- ❑ AEC Q-200 feedthrough BME 0805, X7R, 10nF, 50V for use in 5V lines at 65 °C max.
- ❑ 300 samples passed monitored BI at 125 °C/100V/160hr with zero failures.
- ❑ Monitored LT of 60 soldered samples at 125 °C/100V/2000hr resulted in 2 failures.



- ✓ For some AEC-Q200 parts BI is not necessary.
- ✓ Conservative estimations showed that at the mission conditions TTF > 10,000 years.
- ✓ Parts failing MIL life test requirements can be used for a space mission at substantially derated conditions.



# Lessons Learned

- ❑ Instead of qualifying a COTS capacitor “for space”, we need to ensure that a given batch of parts has an acceptable probability of failure at specific application conditions for the required mission time.
- ❑ Paradigm shift: reliability for the mission instead of compliance with MIL-spec (relaxed?) requirements.
- ❑ Development of S&Q plans for COTS capacitors should include:
  - Analysis of potential reliability concerns specific to the design.
  - Qualification testing using sufficiently large SS of soldered capacitors.
  - Analysis of application conditions.
  - Assessments of reliability acceleration factors.
- ❑ COTS+ capacitors require BI, unless opposite is proven statistically.